A pragmatic methodology to abstract the EDZ around tunnels of a geological radioactive waste repository. Application to the HG-A experiment in Mont Terri.

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Outline

Context

- Radioactive waste in CH
- The need for abstracted models
- Methodology
- Application. HG-A experiment
- Concluding remarks



1. Context. Radioactive waste in Switzerland

Sites for the disposal of radioactive waste in CH. Target = OPA



Provisional Safety Analysis (SA) on long term repository induced effects:

- pH plume back-fill of L/ILW caverns.
- accumulation and release of repository gases.
- heat emission of HLW canisters.
- Excavation Damaged Zone (EDZ) around back-filled structures.



1. Context. The need for abstracted models

 Traditional THM models not wellsuited to Safety Analysis either due to simplicity (e.g., piece-wise homogeneous) or complexity (long model runs, etc.).



Lanyon et al. (2009)

- SA demands models that are:
 - Simple and fast
 - Plausible
 - Heuristic, based on physical processes
 - Validated
- Prior work (EAGE Porto, 2014): EDZ abstraction methodology.

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2. Methodology. Upscaling





FEMDEM

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$$K = K_m + K_f$$

K

COMPOSITE

2. Methodology. Temporal evolution of parameters

Resaturation of fractures :

- (1) $\Delta p>0$, from p_{atm} to $p_h \rightarrow$ decrease of $\sigma_n' \rightarrow$ fracture closure $\rightarrow K_f$ and ϕ_f decrease
- (2) Matrix is clay rich -> swelling. K_m and ϕ_m increase

Overall, reduction of EDZ transmissivity



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2. Methodology. Temporal evolution of parameters

At each time step:

(1) Calculate fracture aperture from pressure (effective stress) :

$$b(t) = b_0 - \frac{1}{b_0 K_{n0} \Delta p(t)^{\alpha - 1} + 1}$$

Modified Barton-Bandis' model α : closure rate

- (2) Recalculate fracture transmissivity and porosity and upscale to grid: K_f and ϕ_f
- (3) Assuming that total porosity ϕ does not change in time, calculate ϕ_m :

$$\phi_m = \frac{\phi - \phi_f}{1 - \phi_f}$$

(4) Calculate Km from ϕ_m using Kozeny-Carman equation:

$$K_m(t) = \frac{\phi_m(t)^3}{(1 - \phi_m(t))^2} \cdot \frac{\rho \cdot g}{\mu} \cdot \frac{d_{10}^2}{180}$$

(5) Recalculate total $K = K_f + K_m$ and simulate pressure with updated fields

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Analysis	Reference
Response to excavation	Marschall et al., 2006 and 2008
Test section saturation and hydraulic testing	Lanyon et al., 2009
Gas testing	Lanyon et al., 2014



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Different FEMDEMS mimicking different local stress conditions



Model discretization, boundary conditions and extent







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- Calibration parameters (not exhaustive search, but trial and error):
 - α , the rate of fracture closure. Low α = high rate of closure.
 - β, dampening factor mimicking:
 - the transfer of mechanical energy between megapacker and formation
 - skin effect
- Least squares minimization of misfit at HG-A2 and HG-A3. Model not aimed at fitting perfectly available measurements, but at "ressembling trends". Instead, we seek a heuristic model that is simple, abstractable, based on empirical observations and that captures the physical nature of the phenomenon.
- Local stress conditions highly uncertain. This methodology also allows the selection of the best structural model.









Animation of pressure and of K



End members and abstraction of HG-A



4. Conclusions

- An abstraction methodology to go from extremely complex EDZ models to simple piecewise heterogeneous models, wellsuited to SA.
- Sequential approach: mechanical simulations of EDZ formation and development, then decoupled hydromechanical simulations.

